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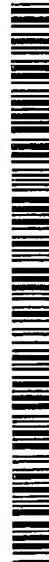
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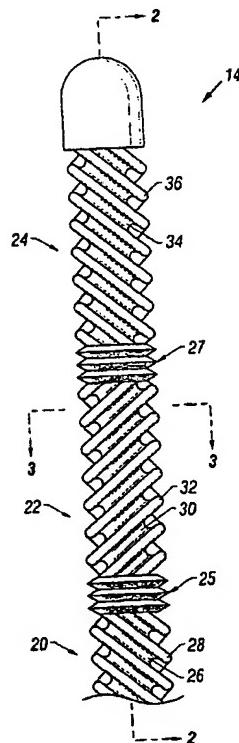
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(54) Title: METHOD OF MANUFACTURING A HEAT TRANSFER ELEMENT FOR IN VIVO COOLING



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(57) Abstract: This invention is a selective organ heat transfer device with a mixing inducing surface (28). The device can have a plurality of elongated, articulated segments, each having a mixing inducing exterior surface. A flexible joint (25) connects adjacent elongated, articulated segments. The device is formed of a mechanical layer such as Ni, and a bio-compatible layer such as Au. An anti-thrombogenic and/or lubricious coating may also be employed for hemo-compatibility. A protective layer such as Au may be employed to provide a degree of non-corrosiveness when exposed to a working fluid.

## METHOD OF MANUFACTURING A HEAT TRANSFER ELEMENT FOR IN VIVO COOLING

### CROSS REFERENCE TO RELATED APPLICATIONS

- 5 This is a continuation-in-part patent application of co-pending U.S. Patent Application Serial No. 09/103,342, filed on 06/23/98, and entitled "Selective Organ Cooling Catheter and Method of Using the Same".

### STATEMENT REGARDING FEDERALLY SPONSORED

#### 10 RESEARCH OR DEVELOPMENT

Not Applicable

### BACKGROUND OF THE INVENTION

Field of the Invention - The present invention relates generally to a method for  
15 manufacturing a heat transfer element that is capable of modification and control of the temperature of a body or of a selected body organ. More particularly, the invention relates to a method for manufacturing an intravascular apparatus including a heat transfer element for controlling body and organ temperature. The invention is also directed to the resulting heat transfer element.

Background Information - Organs in the human body, such as the brain, kidney and heart, are maintained at a constant temperature of approximately 37° C. Hypothermia can be clinically defined as a core body temperature of 35° C or less. Hypothermia is sometimes characterized further according to its severity. A body core temperature in the range of 33° C to 35° C is described as mild hypothermia. A  
25 body temperature of 28° C to 32° C is described as moderate hypothermia. A body core temperature in the range of 24° C to 28° C is described as severe hypothermia.

Hypothermia is uniquely effective in reducing brain injury caused by a variety of neurological insults and may eventually play an important role in emergency brain resuscitation. Experimental evidence has demonstrated that cerebral cooling  
30 improves outcome after global ischemia, focal ischemia, or traumatic brain injury.

For this reason, hypothermia may be induced in order to reduce the effect of certain bodily injuries to the brain as well as other organs.

Catheters have been developed which are inserted into the bloodstream of the patient in order to induce total body hypothermia. For example, U.S. Patent No. 5 3,425,419 to Dato describes a method and apparatus of lowering and raising the temperature of the human body. Dato induces moderate hypothermia in a patient using a metallic catheter. The metallic catheter has an inner passageway through which a fluid, such as water, can be circulated. The Dato catheter has an elongated cylindrical shape and is constructed from stainless steel. For example, Dato suggests 10 the use of a catheter approximately 70 cm in length and approximately 6 mm in diameter. It is clear that the Dato device has numerous limitations. For example, such a catheter would likely be inflexible and unable to navigate a tortuous 15 vasculature.

Cooling helmets or head gear have also been used in an attempt to cool only 15 the head rather than the patient's entire body. However, such methods rely on conductive heat transfer through the skull and into the brain. One drawback of using 20 conductive heat transfer is that the process of reducing the temperature of the brain is prolonged. Also, it is difficult to precisely control the temperature of the brain when using conduction due to the temperature gradient that must be established externally 25 in order to sufficiently lower the internal temperature. From a practical standpoint, such devices are cumbersome and may make continued treatment of the patient difficult or impossible.

Selected organ hypothermia has been accomplished using extracorporeal perfusion, as detailed by Arthur E. Schwartz, M.D. et al., in *Isolated Cerebral 25 Hypothermia by Single Carotid Artery Perfusion of Extracorporeally Cooled Blood in Baboons*, NEUROSURGERY, vol. 39, no. 3, p. 577 (September, 1996). However, external circulation of blood is not a practical approach for treating humans because the risk of infection, need for anticoagulation, and risk of bleeding is too great.

In all of the above, the devices have tended to have inelegant constructions, 30 which have neglected some of the subtleties of hemocompatibility and flexibility. Therefore, a practical method to manufacture an apparatus, which is capable of modifying and controlling the temperature of a selected organ, satisfies a long-felt need.

### BRIEF SUMMARY OF THE INVENTION

In one aspect, the invention is directed towards a heat transfer device including a flexible mechanical layer of a metal that is shaped and configured to produce mixing in fluid flowing adjacent the layer, and a biocompatible layer of material disposed adjacent the mechanical layer.

Implementations of the invention may include one or more of the following. A protective layer may be provided that is formed of a material that is not corrosive when exposed to a working fluid, the protective layer disposed on the side of the mechanical layer opposite the biocompatible layer. A top layer of a material, chosen from the group consisting essentially of heparin, similar antithrombogenic materials and lubricious materials, may be disposed on the side of the biocompatible layer opposite the mechanical layer.

The mechanical layer may be formed of a sandwich structure including at least two layers of materials. The sandwich structure may be formed of two layers of a first material separated by a layer of a second material. The thickness of all the layers together may be less than about 1 mil in thickness. The layers of the first material may each have substantially the same thickness. The first material may be selected from the group consisting essentially of Ni, Fe, Ti, steel, Al, or other similar materials, or combinations of the same, and the second material may be selected from the group consisting essentially of Ag, Au, Cu, or other similar materials, or combinations of the same. The total diameter of the device may be between about 9 french [f] to 14 f. The heat transfer device may include heat transfer segments separated by articulating joints. The segments may be shaped and configured as helices and the joints as bellows or flexible tubes. The biocompatible coating may be selected from the group consisting essentially of Au, parylene, platinum, other similar materials, and combinations thereof. The mechanical layer may have a thermal conductivity in the range of about 0.1 to 4 W/cm-K. A protective layer may be the innermost layer, the protective layer formed of a material which is non-corrosive when exposed to a working fluid. For working fluids of saline, the protective layer may be, e.g., Au.

In another aspect, the invention may be directed to a method of making a heat transfer device, including disposing a mandrel in a deposition apparatus, the mandrel

having an outside shape such that a material formed thereon is configured and arranged to cause mixing in a fluid flowing adjacent the material. Other steps include depositing a mechanical layer of a material having sufficient ductility and surface energy to substantially conform to the contours of the outside shape, depositing a  
5 biocompatible coating on the mechanical layer, and dissolving the mandrel.

Implementations of the method may include one or more of the following. Either or both of a layer of an antithrombogenic material or a lubricious material may be deposited on the biocompatible coating. A protective layer may be deposited on the mandrel so as to be the innermost layer of the device, the protective layer formed  
10 of a material which does not corrode when exposed to a working fluid, such as Au. The biocompatible coating may be selected from the group consisting essentially of Au, Pt, urethane, Teflon®, other noble metals, parylene, or other similar materials or combinations thereof. The mandrel may be formed of Al, and may be formed having a shape configured and arranged such that a material formed thereon is capable of  
15 causing mixing in a fluid flowing adjacent the material. The mandrel may be formed by a technique selected from the group consisting of machining, injection molding, laser machining, hydroforming, or other similar techniques. The surface of the heat transfer device may be bombarded with nitrogen to provide a degree of thrombogenicity either in combination with or instead of an antithrombogenic coating  
20 such as heparin. In all of the above, the depositing may be performed by a technique selected from the group consisting of CVD, PVD, sputtering, MBE, electroplating, electrochemical deposition [ECD], or other similar techniques or combinations of the above. A seed layer may be deposited on the mandrel, the seed layer formed of a material which is capable of bonding to the protective layer or to the mechanical  
25 layer. The depositing a mechanical layer may include depositing a sandwich structure. The depositing a sandwich structure may include depositing a layer of a first metal, depositing a layer of a second metal, and then depositing another layer of the first metal. The first metal may be Ni and the second metal may be Cu.

Advantages of the invention are manyfold. A highly conductive metallic heat  
30 transfer element may be manufactured conveniently. The metallic heat transfer element may retain a high degree of flexibility so as to be able to navigate tortuous vasculature. The heat transfer element has an atraumatic profile and is biocompatible.

**BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWINGS**

The novel features of this invention, as well as the invention itself, will be best understood from the attached drawings, taken along with the following description, in which similar reference characters refer to similar parts, and in which:

- 5       Figure 1 is an elevation view of an embodiment of a heat transfer element according to the invention;
- Figure 2 is longitudinal section view of the heat transfer element of Figure 1;
- Figure 3 is a transverse section view of the heat transfer element of Figure 1;
- Figure 4 is a cut-away perspective view of an alternative embodiment of a heat  
10      transfer element according to the invention;
- Figure 5 is a transverse section view of the heat transfer element of Figure 4;
- Figure 6 is a schematic representation of layers constituting a wall of the heat transfer element according to an embodiment of the invention and formed by a method according to the invention;
- 15      Figure 7 is a schematic representation of layers constituting a wall of the heat transfer element according to a second embodiment of the invention and formed by a method according to the invention; and
- Figure 8 is an exploded schematic representation of layers constituting a wall of the heat transfer element according to a third embodiment of the invention and  
20      formed by a method according to the invention.

**DETAILED DESCRIPTION OF THE INVENTION**

- In order to regulate the temperature of a selected organ intravascularly, a heat transfer element may be placed in the feeding artery of the organ to absorb or deliver heat from or to the blood flowing into the organ. The transfer of heat may cause either a cooling or a heating of the selected organ. The heat transfer element must be small enough to fit within the feeding artery while still allowing a sufficient blood flow to reach the organ in order to avoid ischemic organ damage. A heat transfer element that selectively cools an organ should be capable of providing the necessary  
25      heat transfer rate to produce the desired cooling or heating effect within the organ. By placing the heat transfer element within the feeding artery of an organ, the temperature of an organ can be controlled without significantly affecting the remaining parts of the body. In contrast, by placing the heat transfer element in a  
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large vein, such as the superior vena cava, total body cooling can be effected in a manner which avoids the deleterious consequences of prior art total body cooling.

To selectively cool the brain, for example, the heat transfer element is placed into the common carotid artery, or both the common carotid artery and the internal carotid artery. The internal diameter of the common carotid artery ranges from 6 to 8 mm and the length ranges from 80 to 120 mm. Thus, the heat transfer element residing in one of these arteries cannot be much larger than 10 f in diameter in order to avoid occluding the vessel. For placement in the superior vena cava, the size of the heat transfer element may be much larger, e.g., 14 f.

It is important that the heat transfer element be flexible in order to be placed within the small feeding artery of an organ. Feeding arteries, like the carotid artery, branch off the aorta at various levels. Subsidiary arteries continue to branch off the initial branches. For example, the internal carotid artery is a small diameter artery that branches off of the common carotid artery near the angle of the jaw. Because the heat transfer element is typically inserted into a peripheral artery, such as the femoral artery, and accesses the feeding artery by initially passing through a series of one or more of these branches, the flexibility of the heat transfer element is an important characteristic of the heat transfer element. Further, the heat transfer element is ideally constructed from a highly thermally conductive material such as metal in order to facilitate heat transfer. The use of a highly thermally conductive material increases the heat transfer rate for a given temperature differential between the coolant within the heat transfer element and the blood. This facilitates the use of a higher temperature coolant within the heat transfer element, allowing safer coolants, such as water, to be used. Highly thermally conductive materials, such as metals, tend to be rigid. Therefore, the design of the heat transfer element should facilitate flexibility in an inherently inflexible material. More details of the construction of the heat transfer element are disclosed below.

In order to obtain the benefits of hypothermia described above, it is desirable to reduce the temperature of the blood flowing to the brain (or alternatively for total body cooling, to the blood flowing out of the heart) to between 30° C and 32° C. Given that a typical brain has a blood flow rate through each carotid artery (right and left) of approximately 250-375 cubic centimeters per minute, the heat transfer element should absorb 75-175 Watts of heat when placed in one of the carotid arteries, in

order to induce the desired cooling effect. It should be noted that smaller organs may have less blood flow in the supply artery and may require less heat transfer, such as 25 Watts. For total body cooling, rates of 250-300 Watts may be required.

The magnitude of the heat transfer rate is proportional to the surface area of  
5 the heat transfer element, the temperature differential, and the heat transfer coefficient of the heat transfer element.

As noted above, the receiving vessel into which the heat transfer element is placed has a limited diameter and length. Thus, surface area of the heat transfer element must be limited, to avoid significant obstruction of the vessel, and to allow  
10 the heat transfer element to pass easily through the vascular system. For placement within the internal and common carotid artery, the cross sectional diameter of the heat transfer element is limited to about 4 mm, and its length is limited to approximately 10 cm. Other vessels may have different requirements. For example, for placement within the superior vena cava to effect total body cooling, the cross sectional diameter  
15 of the heat transfer element may be considerably larger, e.g., 12 f, 14 f, 16 f, 18 f, 20 f, or even more.

The mechanisms by which the value of the convection heat transfer coefficient may be increased are complex. However, it is known that the convection heat transfer coefficient increases with the level of turbulent kinetic energy in the fluid flow. Thus  
20 it is advantageous to have turbulent blood flow in contact with the heat transfer element. For reasons given in the parent cases of this application, turbulent flow, or at least mixing flow, can be induced using surface features on the heat transfer element. This flow can be induced both in the blood and in the working fluid. The surface features may be, as disclosed below, counter-rotating helices, non-counter-rotating  
25 helices, staggered or non-staggered protuberances, etc.

In particular, to create the desired level of mixing intensity in the blood, one embodiment of the invention uses a modular design. This design creates helical blood flow and produces a high level of mixing in the free stream by periodically forcing abrupt changes in the direction of the helical blood flow. Figure 1 is a side view of  
30 such a mixing inducing heat transfer element which may be employed within an artery or vein. The abrupt changes in flow direction are achieved through the use of a series of two or more heat transfer segments, each comprised of one or more helical ridges.

The use of periodic abrupt changes in the helical direction of the blood flow in order to induce mixing may be illustrated with reference to a common clothes washing machine. The rotor of a washing machine spins initially in one direction causing laminar flow. When the rotor abruptly reverses direction, significant kinetic  
5 energy is created within the wash basin as the changing currents cause random mixing motion within the clothes-water slurry.

Referring to Figure 1, the heat transfer element 14 is comprised of a series of elongated, articulated segments or modules 20, 22, 24. Three such segments are shown in this embodiment, but two or more such segments could be used without  
10 departing from the spirit of the invention. As seen in Figure 1, a first elongated heat transfer segment 20 is located at the proximal end of the heat transfer element 14. A mixing-inducing exterior surface of the segment 20 comprises four parallel helical ridges 28 with four parallel helical grooves 26 therebetween. One, two, three, or more parallel helical ridges 28 could also be used without departing from the spirit of the  
15 present invention. In this embodiment, the helical ridges 28 and the helical grooves 26 of the heat transfer segment 20 have a left-hand twist, referred to herein as a counter-clockwise spiral or helical rotation, as they proceed toward the distal end of the heat transfer segment 20.

The first heat transfer segment 20 is coupled to a second elongated heat  
20 transfer segment 22 by a first bellows section 25, which provides flexibility and compressibility. The second heat transfer segment 22 comprises one or more helical ridges 32 with one or more helical grooves 30 therebetween. The ridges 32 and grooves 30 have a right hand, or clockwise, twist as they proceed toward the distal end of the heat transfer segment 22. The second heat transfer segment 22 is coupled  
25 to a third elongated heat transfer segment 24 by a second bellows section 27. The third heat transfer segment 24 comprises one or more helical ridges 36 with one or more helical grooves 34 therebetween. The helical ridge 36 and the helical groove 34 have a left hand, or counter-clockwise, twist as they proceed toward the distal end of the heat transfer segment 24. Thus, successive heat transfer segments 20, 22, 24 of  
30 the heat transfer element 14 alternate between having clockwise and counterclockwise helical twists. The actual left or right hand twist of any particular segment is immaterial, as long as adjacent segments have opposite helical twists.

In addition, the rounded contours of the ridges 28, 32, 36 also allow the heat transfer element 14 to maintain a relativelyatraumatic profile, thereby minimizing the possibility of damage to the blood vessel wall. A heat transfer element according to the present invention may be comprised of one, two, three, or more heat transfer  
5 segments.

The bellows sections 25, 27 are formed from seamless and nonporous materials, such as metal, and therefore are impermeable to gas, which can be particularly important, depending on the type of working fluid which is cycled through the heat transfer element 14. The structure of the bellows sections 25, 27  
10 allows them to bend, extend and compress, which increases the flexibility of the heat transfer element 14 so that it is more readily able to navigate through blood vessels. The bellows sections 25, 27 also provide for axial compression of the heat transfer element 14, which can limit the trauma when the distal end of the heat transfer element 14 abuts a blood vessel wall. The bellows sections 25, 27 are also able to  
15 tolerate cryogenic temperatures without a loss of performance. The bellows sections may be replaced with flexible tubes or thin-walled metal or polymers. In an alternative embodiment, the bellows may be replaced by helical springs which are then coated with a polymer to make a fluid-tight seal. As it is believed that the majority of the heat transfer is through the heat transfer segments, as opposed to the  
20 bellows, such an embodiment would be unlikely to unduly affect the heat transfer.

Figure 2 is a longitudinal sectional view of the heat transfer element 14 of an embodiment of the invention, taken along line 2-2 in Figure 1. Some interior contours are omitted for purposes of clarity. An inner tube 42 creates an inner coaxial lumen 40 and an outer coaxial lumen 46 within the heat transfer element 14. Once the heat  
25 transfer element 14 is in place in the blood vessel, a working fluid such as saline or other aqueous solution may be circulated through the heat transfer element 14. Fluid flows up a supply catheter into the inner coaxial lumen 40. At the distal end of the heat transfer element 14, the working fluid exits the inner coaxial lumen 40 and enters the outer lumen 46. As the working fluid flows through the outer lumen 46, heat is  
30 transferred from the working fluid to the exterior surface 37 of the heat transfer element 14. Because the heat transfer element 14 is constructed from a high conductivity material as explained in more detail below, the temperature of its exterior surface 37 may reach very close to the temperature of the working fluid. The

tube 42 may be formed as an insulating divider to thermally separate the inner lumen 40 from the outer lumen 46. For example, insulation may be achieved by creating longitudinal air channels in the wall of the insulating tube 42. Alternatively, the insulating tube 42 may be constructed of a non-thermally conductive material like 5 polytetrafluoroethylene or another similar polymer.

It is important to note that the same mechanisms that govern the heat transfer rate between the exterior surface 37 of the heat transfer element 14 and the blood also govern the heat transfer rate between the working fluid and the interior surface 38 of the heat transfer element 14. The heat transfer characteristics of the interior surface 10 38 are particularly important when using water, saline or other fluid which remains a liquid as the coolant. Other coolants, such as freon, undergo nucleate boiling and create mixing through a different mechanism. Saline is a safe coolant because it is non-toxic, and leakage of saline does not result in a gas embolism, which could occur with the use of boiling refrigerants. Since mixing in the coolant is enhanced by the 15 shape of the interior surface 38 of the heat transfer element 14, the coolant can be delivered to the heat transfer element 14 at a warmer temperature and still achieve the necessary heat transfer rate.

This has a number of beneficial implications in the need for insulation along the catheter shaft length. Due to the decreased need for insulation, the catheter shaft 20 diameter can be made smaller. The enhanced heat transfer characteristics of the interior surface of the heat transfer element 14 also allow the working fluid to be delivered to the heat transfer element 14 at lower flow rates and lower pressures. High pressures may make the heat transfer element 14 stiff and cause it to push 25 against the wall of the blood vessel, thereby shielding part of the exterior surface 37 from the blood. Because of the increased heat transfer characteristics achieved by the alternating helical ridges 28, 32, 36, the pressure of the working fluid may be as low as 5 atmospheres, 3 atmospheres, 2 atmospheres or even less than 1 atmosphere.

Figure 3 is a transverse sectional view of the heat transfer element 14 according to an embodiment of the invention, taken at a location denoted by the line 30 3-3 in Figure 1. Figure 3 illustrates a five-lobed embodiment, whereas Figure 1 illustrates a four-lobed embodiment. As mentioned earlier, any number of lobes might be used. In Figure 3, the coaxial construction of the heat transfer element 14 is clearly shown. The inner coaxial lumen 40 is defined by the insulating coaxial tube

42. The outer lumen 46 is defined by the exterior surface of the insulating coaxial tube 42 and the interior surface 38 of the heat transfer element 14. In addition, the helical ridges 32 and helical grooves 30 may be seen in Figure 3.

As noted above, in the preferred embodiment, the depth of the grooves,  $d_i$ ,  
5 may be greater than the boundary layer thickness which would have developed if a cylindrical heat transfer element were introduced. For example, in a heat transfer element 14 with a 4 mm outer diameter, the depth of the invaginations,  $d_i$ , may be approximately equal to 1 mm if designed for use in the carotid artery.

Although Figure 3 shows four ridges and four grooves, the number of ridges  
10 and grooves may vary. Thus, heat transfer elements with 1, 2, 3, 4, 5, 6, 7, 8 or more ridges are specifically contemplated.

Referring back to Figure 1, the heat transfer element 14 has been designed to address all of the design criteria discussed above. First, the heat transfer element 14 is flexible and is made of a highly conductive material. The flexibility is provided by a  
15 segmental distribution of bellows sections 25, 27 that provide an articulating mechanism. Bellows have a known convoluted design that provides flexibility. Second, the exterior surface area 37 has been increased through the use of helical ridges 28, 32, 36 and helical grooves 26, 30, 34. The ridges also allow the heat transfer element 14 to maintain a relatively atraumatic profile, thereby minimizing the  
20 possibility of damage to the vessel wall. Third, the heat transfer element 14 has been designed to promote turbulent kinetic energy both internally and externally. The modular or segmental design allows the direction of the invaginations to be reversed between segments. The alternating helical rotations create an alternating flow that results in mixing the blood in a manner analogous to the mixing action created by the  
25 rotor of a washing machine that switches directions back and forth. This mixing action is intended to promote high level turbulent kinetic energy to enhance the heat transfer rate. The alternating helical design also causes beneficial mixing, or turbulent kinetic energy, of the working fluid flowing internally.

Figure 4 is a cut-away perspective view of an alternative embodiment of a heat  
30 transfer element 50. An external surface 52 of the heat transfer element 50 is covered with a series of axially staggered protrusions 54. The staggered nature of the outer protrusions 54 is readily seen with reference to Figure 5 which is a transverse cross-

sectional view taken at a location denoted by the line 5-5 in Figure 4. In order to induce free stream mixing, the height,  $d_p$ , of the staggered outer protrusions 54 may be greater than the thickness of the boundary layer which would develop if a smooth heat transfer element had been introduced into the blood stream. As the blood flows along 5 the external surface 52, it collides with one of the staggered protrusions 54 and a turbulent wake flow is created behind the protrusion. As the blood divides and swirls along side of the first staggered protrusion 54, its turbulent wake encounters another staggered protrusion 54 within its path preventing the re-lamination of the flow and creating yet more mixing. In this way, the velocity vectors are randomized and 10 mixing is created not only in the boundary layer but also in at least a portion of the free stream. As is the case with the preferred embodiment, this geometry also induces a mixing effect on the internal coolant flow.

In use, a working fluid is circulated up through an inner coaxial lumen 56 defined by an insulating coaxial tube 58 to a distal tip of the heat transfer element 50. 15 The working fluid then traverses an outer coaxial lumen 60 in order to transfer heat to the exterior surface 52 of the heat transfer element 50. The inside surface of the heat transfer element 50 is similar to the exterior surface 52 in order to induce mixing flow of the working fluid. The inner protrusions can be aligned with the outer protrusions 54, as shown in Figure 5, or they can be offset from the outer protrusions 54, as 20 shown in Figure 4.

The heat transfer element can absorb or provide over 75 Watts of heat to the blood stream and may absorb or provide as much as 100 Watts, 150 Watts, 170 Watts, 250 Watts, 300 Watts, or more. For example, a heat transfer element with a diameter of 4 mm and a length of approximately 10 cm using ordinary saline solution chilled so 25 that the surface temperature of the heat transfer element is approximately 5° C and pressurized at 2 atmospheres can absorb about 100 Watts of energy from the bloodstream. Smaller geometry heat transfer elements may be developed for use with smaller organs which provide 60 Watts, 50 Watts, 25 Watts or less of heat transfer.

The method of manufacturing a heat transfer element will now be described in 30 more detail. The exterior structure of the heat transfer element is of a complex shape as has been described in order to induce mixing in the flow of blood around the heat transfer element, as well as to induce mixing in the flow of working fluid within the heat transfer element. As may be clear, many varieties and shapes may be employed

to cause such flow. Such shapes are termed herein as "mixing-inducing shapes". Examples of mixing-inducing shapes include: helical, alternating helical or other enantiomeric shapes, aberration-including shapes, bump-including shapes, channel-including shapes, crenellated shapes, hook- or horn- shapes, labyrinthine shapes, and 5 any other shapes capable of inducing mixing. Thus, the metallic element or elements or compounds forming the heat transfer element must be sufficiently ductile to assume such shapes during deposition.

It is further noted here that while the generic term "deposition" is used, this term is intended broadly to cover any process in which metals or coating may be 10 disposed on a mandrel or other layer of a heat transfer element. For example, deposition may include: CVD, PVD, sputtering, MBE, forms of crystal or amorphic material "growth", spray coating, electroplating, ECD, and other methods which may be employed to form a mandrel or a coating having a mixing-inducing shape. Methods such as ECD and electroplating have the benefit of having a charged 15 workpiece – this charge may be employed to fix the workpiece to the tool.

In general, the processes which may be employed to form the heat transfer element include forming a mandrel having a mixing inducing shape, coating the mandrel with a metal layer or a series of layers (i.e., the heat transfer element), and dissolving the mandrel.

20 A first step in the process of forming a heat transfer element may be to form a mandrel. One type of mandrel may be made of aluminum such as Al 6061 with a T6 heat treatment. Aluminum is useful because the same is capable of being dissolved or leached out easily with a caustic soda. A hole disposed along the axis of the heat transfer element may speed such leaching. The mandrel may be formed by machining 25 such as by a Citizen Swiss Screw Machine. The mandrel may also be made via injection molding if the same is made of plastic, wax, low-melting-temperature thermoplastics, and the like. Other methods which may be employed to form the mandrel include machining via laser (note that laser forming is typically only employed for the outside of an element), hydroforming, and other similar methods.

30 However the mandrel is formed, it is important for the same to have a smooth surface finish and exterior texture. In this way, the resulting heat transfer element will be smooth. A smooth mandrel allows an atraumatic device to be formed around the same. A smooth mandrel also allows a smooth metallic coating (heat transfer

element) to be simply deposited around the same thus ensuring uniform heat transfer, a constant thickness of biocoating, an atraumatic profile, etc.

A basic series of coating layers is shown in Figure 6. Figure 6 shows a mechanical layer 104, typically made of a metal, and a biocompatible layer 106. The 5 mechanical layer 104 is the basic conductive element. The mechanical layer 104 is responsible for heat conduction to provide cooling and thus should have a thermal conductivity in the range of about 0.1 to 4 W/cm-K, so long as such materials can be deposited. Typical metals which may be employed for the mechanical layer 104 include Ni, Cu, Au, Ag, Ti, Ta, nitinol, stainless steel, etc. or combinations of these or 10 other similar elements. The thickness of the mechanical layer should be less than about 2 mils thick to allow for sufficient flexibility to navigate tortuous vasculature, although this is strongly dependent on the type of metal and on the tortuosity of the vasculature involved. Regarding the type of metal, any noble metal may be employed. Certain of these have deleterious biocompatibility, however, and each has 15 different manufacturing concerns. For example, a Au heat transfer element would require a seed layer since Au will not stick to the Al mandrel.

Ni has been found to be useful. Cu is also useful and has a high conductivity; unfortunately, Cu is also likely to assume the form of the vasculature in which the same is disposed.

20 For sake of argument, it is assumed here that Ni forms the basic heat transfer element. As stated above, Ni is not hemocompatible. Thus, a biocompatible layer 106 is disposed on the mechanical layer 104 as is shown in Figure 6. The biocompatible layer may be, e.g., urethane, parylene, Teflon®, a lubricious coating, an antithrombogenic coating such as heparin, a noble metal such as Au, or 25 combinations of the above or other similar materials.

One difficulty with the above embodiment may be that, with use of certain working fluids, such as saline, corrosion of the mechanical layer may occur. In the case of a mechanical layer 104 of Ni, saline may be especially corrosive. Thus, a protective layer 102 may be employed that is noncorrosive with respect to saline. For 30 example, the protective layer 102 may be made of Au. A Au protective layer 102 may encounter difficulties attaching to an aluminum mandrel, and thus if necessary a layer of Cu may be deposited on the mandrel prior to deposition of the Au layer. Following the dissolution of the mandrel, the Cu layer may also be etched away. The

protective layer may generally be any noble or inert metal, or may be a polymer or other protective material such as Teflon®.

Alternatively, the protective layer 102 may be vacuum deposited, such as by a vapor deposition method, following removal or dissolution of the mandrel. The 5 resulting hole left by the dissolved mandrel allows a path for vaporized gases or liquid chemicals to flow. Thus, materials can be deposited in this fashion on the inside of the heat transfer element. The materials so deposited may be the same as those discussed above: polymers, such as non-corrosive or non-polar polymers, noble metals, and the like.

10 Figure 7 also shows two layers above the mechanical layer 104: a biocompatible layer 106 and a heparin / lubricious layer 108. These may also be combined to form a single biocompatible layer. Alternatively, the biocompatible layer may be a “seed” layer which enhances the connection of the heparin / lubricious layer 108 to the underlying mechanical layer 104. Such a seed layer may be, e.g., 15 parylene. Finally, it should be noted that the heparin / lubricious layer 108 is indicated as exemplary only: either heparin or a lubricious layer may be deposited individually or in combination. For example, in certain applications, heparin may not be necessary.

Another embodiment is shown in Figure 8. This embodiment addresses 20 another difficulty that may occur with various metals. For example, a mechanical layer 104 that is made entirely of Ni may have too low a burst pressure, partially due to its porosity. The protective layer 102 of Figure 7 may address some of these concerns. A better approach may be that shown in Figure 8. In Figure 8, the mechanical layer 104 is broken up into several layers. Two, three, or more layers may 25 be employed. In Figure 8, layers 104a and 104c are formed of a first material such as Ni. An interior layer 104b is deposited between layers 104a and 104c. This layer 104b may be formed of a second material such as Cu. This combination of layers 104a, 104b, and 104c forms a mechanical “sandwich” structure. The Cu layer 104b (the second “metal” or “layer”) may serve to close “pinholes” that may exist within 30 the more porous Ni layers 104a and 104c (the first “metal” or “layer”).

One embodiment that has been found useful is that described by Table I below. In Table I, the biocompatible coating is a noble metal layer of Au. It should be noted that Table I describes a very specific embodiment and is provided purely for

illustrative purposes. Table I should not be construed as limiting. Table I is keyed to Figure 8.

Layer Number	Material	Thickness
102	Au (e.g., mil-g-45204, type one, grade A, class one)	1/10 mil
104a	Ni	3 ½ / 10 to 1 mil
104b	Cu	1/10 mil
104c	Ni	3 ½ / 10 to 1 mil
106	Au	1/10 mil
108	heparin / lubricious	7-10 microns

5        The overall thickness of the group of layers 102-108 may be about 1 mil. The nickel and copper may contain traces of other elements without deleterious consequences.

While the particular invention as herein shown and disclosed in detail is fully capable of obtaining the objects and providing the advantages hereinbefore stated, it is  
10      to be understood that this disclosure is merely illustrative of the presently preferred embodiments of the invention and that no limitations are intended other than as described in the appended claims.

## CLAIMS

We claim:

- 1 1. A heat transfer device, comprising:
  - 2 a flexible mechanical layer of a metal, the mechanical layer shaped and
  - 3 configured to produce mixing in fluid flowing adjacent said
  - 4 layer; and
  - 5 a biocompatible layer of material disposed adjacent said mechanical
  - 6 layer.
- 1 2. The device of claim 1, further comprising a protective layer formed of a  
2 material that is not corrosive when exposed to a working fluid, the protective  
3 layer disposed on the side of the mechanical layer opposite the biocompatible  
4 layer.
- 1 3. The device of claim 1, further comprising a top layer of a material chosen  
2 from the group consisting essentially of antithrombogenic materials and  
3 lubricious materials and combinations thereof, the top layer disposed on the  
4 side of the biocompatible layer opposite said mechanical layer.
- 1 4. The device of claim 3, wherein the combination of layers is less than about 1  
2 mil in thickness.
- 1 5. The device of claim 1, wherein the flexible mechanical layer is selected from  
2 the group consisting essentially of Fe, Ti, Ta, nitinol, stainless steel, Al, Ag,  
3 Au, Cu, and Ni.
- 1 6. The device of claim 1, wherein the total outside diameter of the device is  
2 between about 9 f to 14 f.
- 1 7. The device of claim 1, wherein the heat transfer device includes heat transfer  
2 segments separated by articulating joints.

- 1    8.    The device of claim 7, wherein the segments are shaped and configured as  
2                  helices and the joints are shaped and configured as bellows.
  
- 1    9.    The device of claim 1, wherein the biocompatible coating is selected from the  
2                  group consisting essentially of Au, parylene, platinum, Teflon®, and  
3                  combinations thereof.
  
- 1    10.   The device of claim 3, wherein the antithrombogenic material is heparin.
  
- 1    11.   The device of claim 1, wherein the mechanical layer has a thermal  
2                  conductivity in the range of about 0.1 to 4 W/cm-K.
  
- 1    12.   A method of making a heat transfer device, comprising:  
2                  disposing a mandrel in a deposition apparatus, the mandrel having an outside  
3                  shape such that a layer coating the mandrel is configured and arranged  
4                  to cause mixing in a fluid flowing adjacent said layer;  
5                  depositing a mechanical layer of a material having sufficient ductility and  
6                  surface energy to substantially conform to the contours of the outside  
7                  shape;  
8                  depositing a biocompatible coating on the mechanical layer; and  
9                  dissolving the mandrel.
  
- 1    13.   The method of claim 12, further comprising depositing a layer of an  
2                  antithrombogenic material on the biocompatible coating.
  
- 1    14.   The method of claim 12, further comprising depositing a layer of a lubricious  
2                  material on the biocompatible coating.
  
- 1    15.   The method of claim 12, further comprising depositing a protective layer on  
2                  the mandrel, the protective layer formed of a material which does not corrode  
3                  when exposed to a working fluid.
  
- 1    16.   The method of claim 13, wherein the antithrombogenic material is heparin.

- 1 17. The method of claim 15, wherein the protective layer is Au.
- 1 18. The method of claim 12, wherein the biocompatible coating is selected from  
2 the group consisting essentially of Au, Pt, urethane, Teflon®, a noble metal,  
3 parylene, or combinations thereof.
- 1 19. The method of claim 12, further comprising forming a mandrel, having a  
2 shape configured and arranged such that a material layer coated thereon is  
3 capable of causing mixing in a fluid flowing adjacent said layer, by a  
4 technique selected from the group consisting of machining, injection molding,  
5 laser machining, and hydroforming.
- 1 20. The method of claim 12, further comprising bombarding the surface of the  
2 heat transfer device with nitrogen.
- 1 21. The method of claim 12, wherein said depositing is performed by a technique  
2 selected from the group consisting of CVD, PVD, sputtering, MBE,  
3 electroplating, and ECD.
- 1 22. The method of claim 15, further comprising depositing a seed layer on the  
2 mandrel, the seed layer formed of a material which is capable of bonding to  
3 the protective layer.
- 1 23. The method of claim 12, further comprising depositing a protective layer on  
2 an interior of the mechanical layer, the protective layer formed of a material  
3 which does not corrode when exposed to a working fluid.

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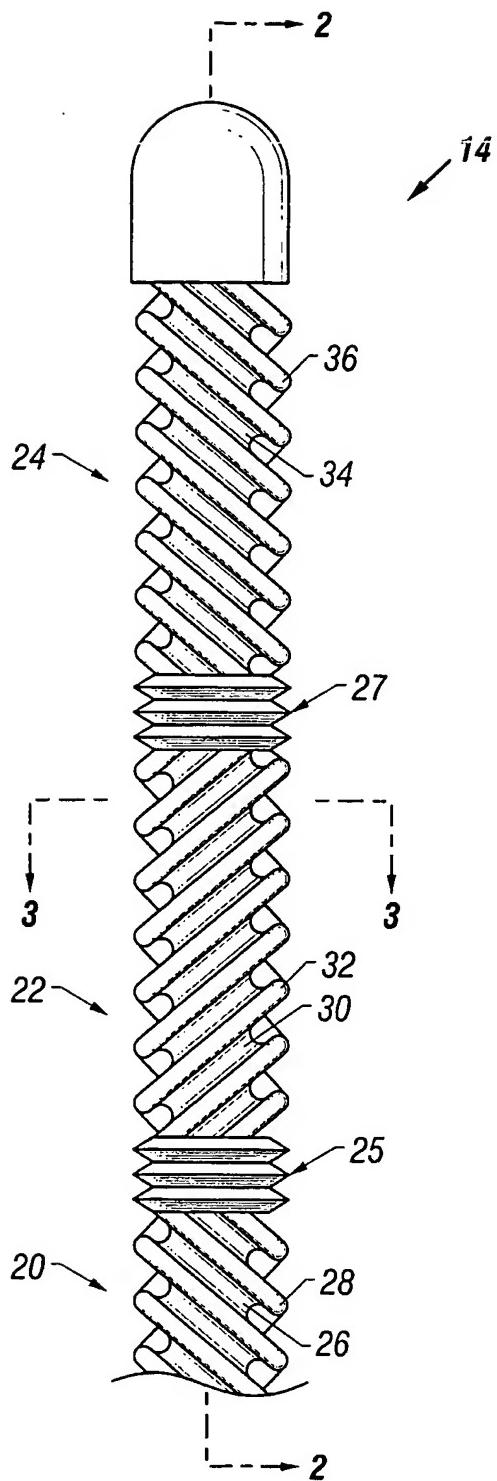


FIG. 1

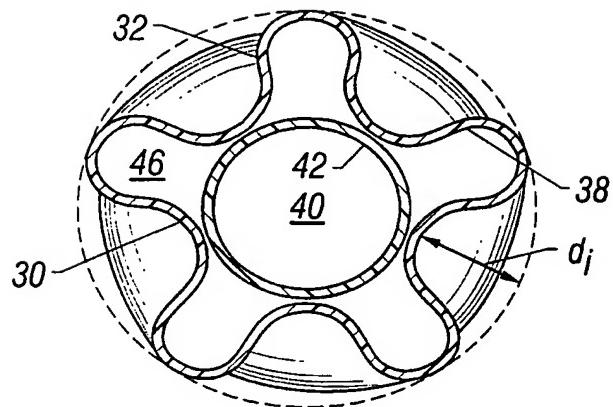
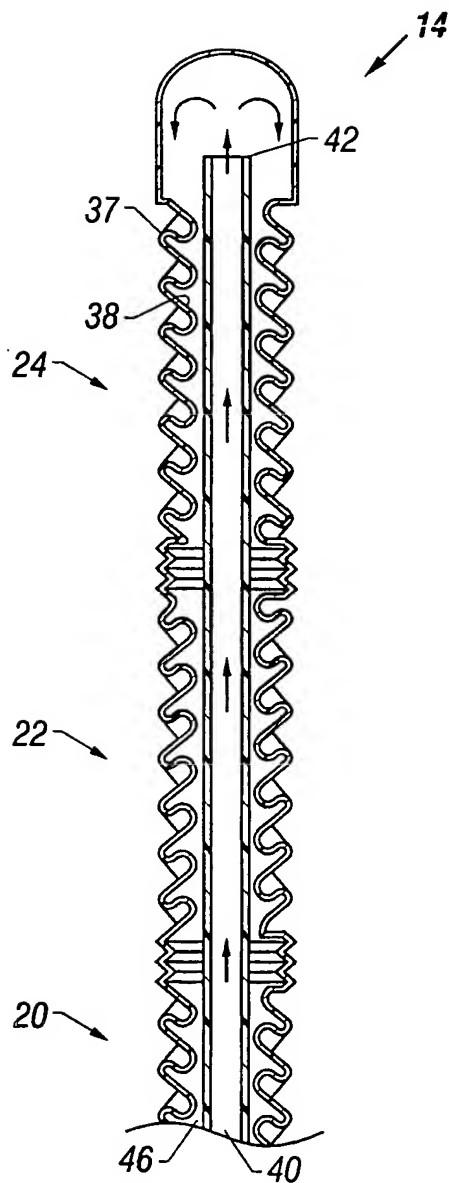


FIG. 3

FIG. 2

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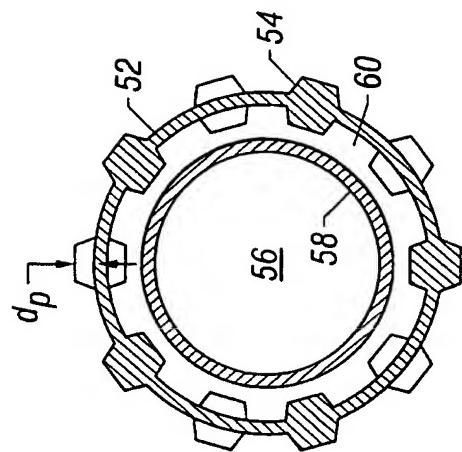


FIG. 5

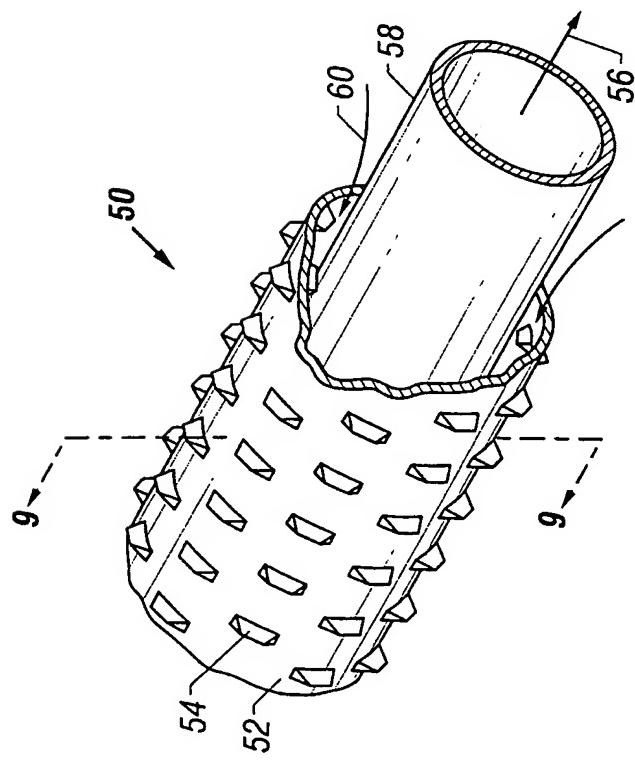


FIG. 4

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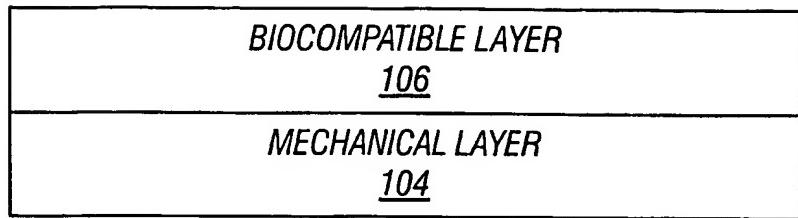


FIG. 6

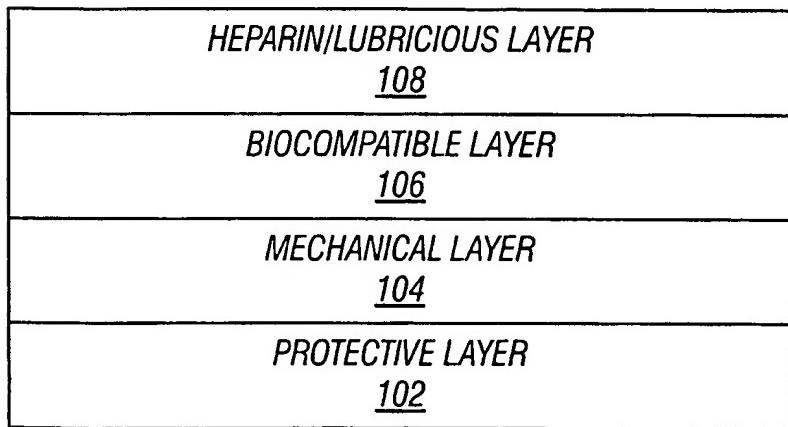


FIG. 7

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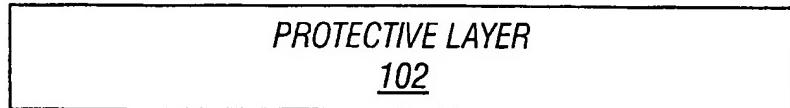
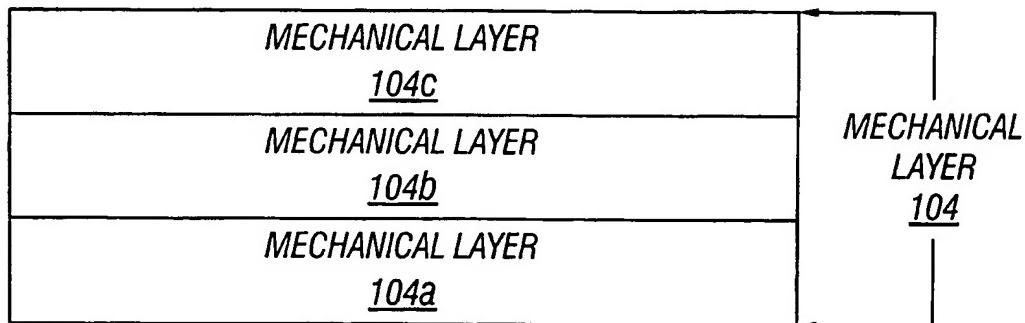
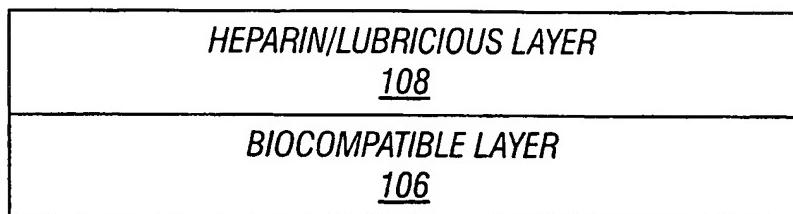


FIG. 8

## INTERNATIONAL SEARCH REPORT

International application No.

PCT/US00/20621

## A. CLASSIFICATION OF SUBJECT MATTER

IPC(7) : A61F 7/00

US CL : 606/20-26

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 606/20-26; 607/105, 106, 113

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 5,899,899 A (ARLESS et al.) 04 May 1999, entire document.	1-23
Y	US 2,913,009 A (KUTHE) 17 November 1959, entire document.	1-23

 Further documents are listed in the continuation of Box C. See patent family annex.

* Special categories of cited documents:	"T"	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"A" document defining the general state of the art which is not considered to be of particular relevance	"X"	document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"E" earlier document published on or after the international filing date	"Y"	document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"&"	document member of the same patent family
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"P" document published prior to the international filing date but later than the priority date claimed		

Date of the actual completion of the international search  
22 SEPTEMBER 2000

Date of mailing of the international search report

04 OCT 2000

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